

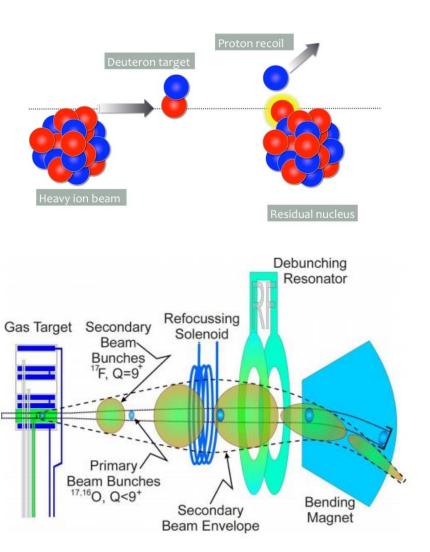
# An RF beam Sweeper for Purifying In-Flight Produced Rare Isotope Beams

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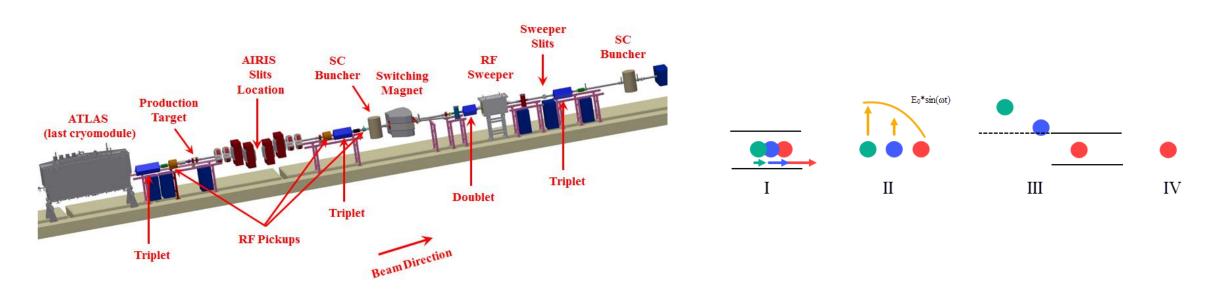
- Background
  - ATLAS is a major US Nuclear Physics facility
    - 200-400 "single users" per year performing experiments
    - Operating 5000-6500 hrs/yr at about 93% efficiency
    - Provides stable beams at high intensity and energy up to 10-20  $\ensuremath{\,\text{MeV}}\xspace/u$
  - In-flight radioactive beams are produced with poor beam properties
    - Secondary radioactive beams are produced when a primary beam hits the target
    - Other low-energy isotopes are produced during this process
    - The isotopes different from the required isotopes must be filtered







- A new inflight radioactive ion separator (AIRIS) will be used to separate and produce secondary radioactive beams from the interaction of ATLAS primary beams in a production target.
  - AIRIS will be at least 10 times more efficient than the existing radioactive
- AIRIS is based on a chicane magnetic fragment separator is to filter the unwanted isotopes,
  - Some isotopes can still pass through this separator
  - Velocity selection criterion is needed





Currently, ATLAS employs a 6 MHz sweeper that provide 50 kV deflection

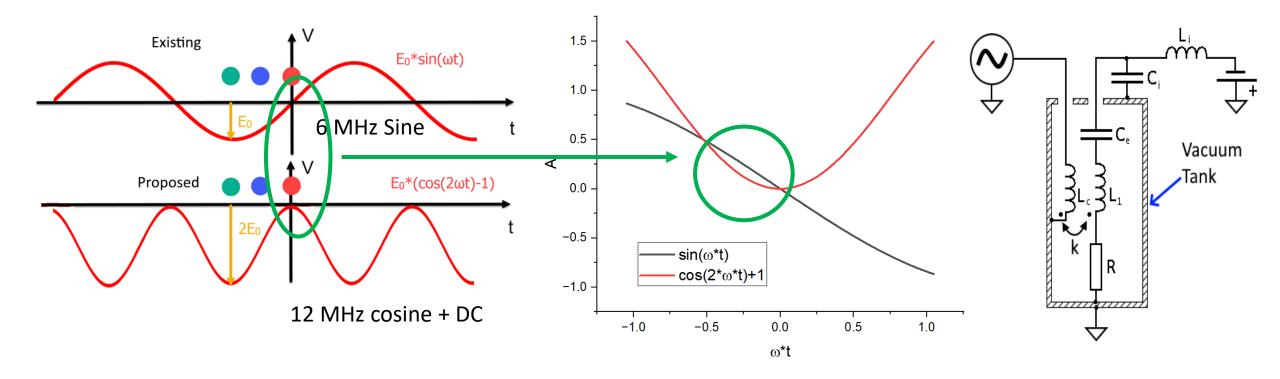
 Many isotopes require higher voltages and frequencies

			RIB Beam	Energy, MeV	Required voltage, kV
			<sup>6</sup> He	80	59
			<sup>11</sup> C	105	21
			<sup>15</sup> C	200	399
			<sup>15</sup> C	65	61
			<sup>17</sup> F	90	28
			<sup>25</sup> Al	180	30
YOUF			<sup>37</sup> K	275	98
	Version	Old		New	
	Frequency, MHz	6.0625	6.0625	12.125	
	Voltage, kV	55	150	150	
	RF power , kW	1	~10	~11	

### Original Phase I idea



- We proposed to increase the frequency by factor of 2 and overlap RF deflection with DC bias to achieve the same deflection as pure 150 kV RF kick at 6 MHz
   – Cosine instead of sine
- Unfortunately, since the cosine wave deflector's zero point is at the crest, it is very much non-linear around it and doesn't provide a good separation



### Phase II sweeper design

 We had to redesign the sweeper to provide purel RF kick (with no bias) of 150 kV that can also operate at 2 frequencies: 6 MHz and 12 MHz for different ion species.

diaBeam

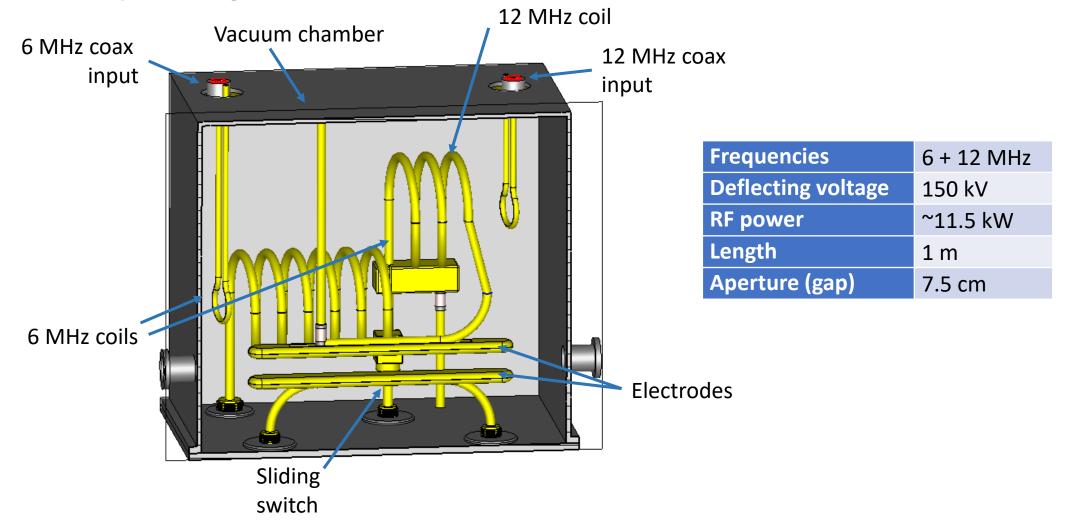
 The frequency should be manually switched between the experiments in ~hours timeframe.

		<5 MeV/u
Fragment purity improvement	>5 times	$E_0 * sin(\omega t)$
Operating frequency	6 and 12 MHz	
Deflecting voltage	150 kV	6 MHz Sine
Secondary beam energy	3-10 MeV/u	>10 MeV/u ► <b>E</b> <sub>0</sub> *sin(2ωt)
Charge-to-mass ratio	varies	$\frown \bigcirc \frown \bigcirc$
Aperture	7.5 cm	
		12 MHz Sine

### Sweeper RF design

 We designed a new sweeper based on 'lumped' elements that allows two operation regimes each providing with 150 kV kick

JiaBeam



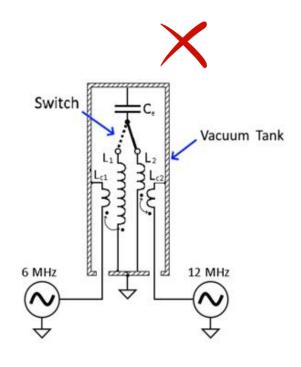
### Design challenges

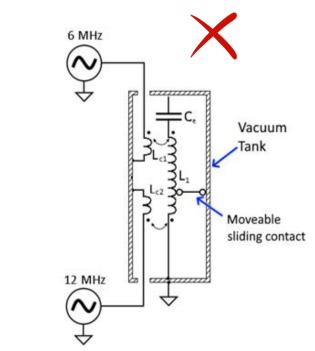


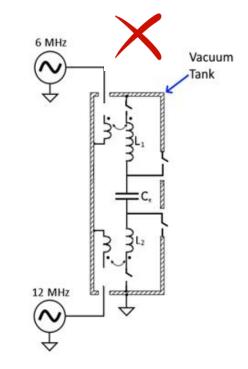
- 1. High peak electric fields
  - Must be kept around 1 Kp at 3x voltage kick
- 2. High RF power losses / heating
  - Scales as ~Voltage<sup>2</sup> (i.e. factor of 10!)
  - Significant enhancement of cooling system
- 3. Two frequencies
  - Two coils
  - Switching mechanism
- 4. Limited footprint
  - Must be fit within the similar-size case to be integrated into ATLAS beamline
  - Must comply with the *existing* space and access restriction for installation
  - Must comply with Argonne safety and reliability requirements
- 5. No RF power source available at ANL
  - To be developed and provided by RadiaBeam

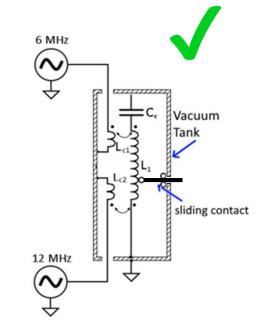
### Dual-frequency operation











- In-vacuum switch:
  - Problem to connect RF and water inside vacuum volume
- Sliding contact:
  - Problem to connect RF and water inside vacuum volume
  - Very large coil

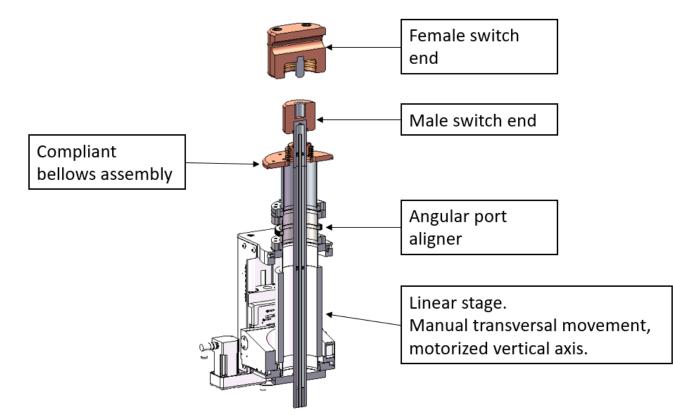
- Ground switches:
  - Allows water flow thru both electrodes
  - RF leakage

- Sliding GND switch:
  - Two separate coils
  - Vacuum, water, mechanical problems are mild

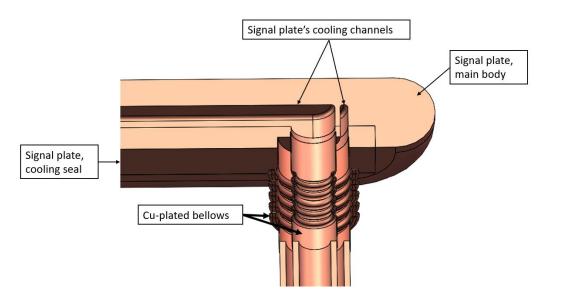
### <sup>10</sup> Energy switch design



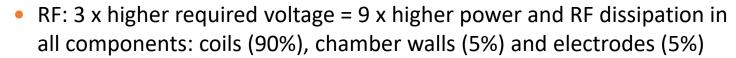
Sliding switch



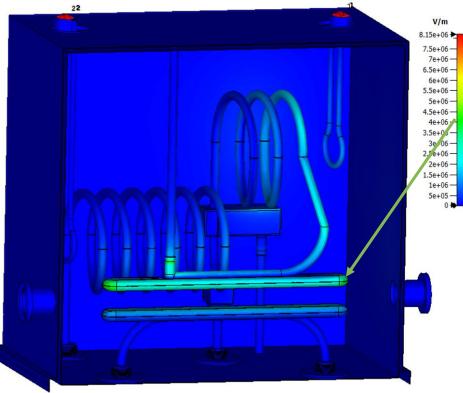
Pipe-in-pipe cooling



### <sup>11</sup> Resonator design considerations



- Water must be run through all current conductors
- Electrodes must have blended shapes to minimize peak E-field on the tips
- Coils dimensions (pipe OD, winding period, major diameter) must be optimized to increase Q
- Mechanical: Large heavy coils and electrodes must be mechanically stable
  - +/- 1mm tolerance on electrode-to-electrode gap
  - Dielectric supports must be introduced to ensure stable electrodes alignment under RF heat load. Alumina is the only option due to low loss and the highest thermal conductivity. MACOR and PEEK have 10x and 100x worse thermal properties.
  - Sliding switch must not deform the coils (and electrode) position during engaging/disengaging
- Vacuum: Avoiding water-to-vacuum braze joints as ATLAS requirement implies making the coils from a single pipe.

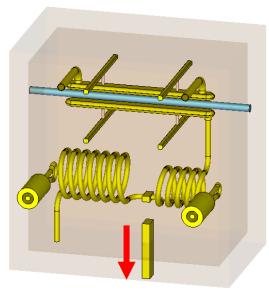


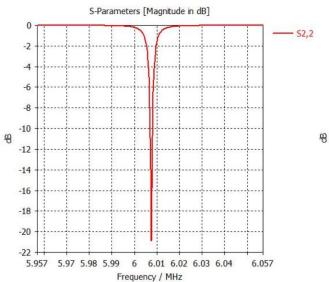
aBeam

### <sup>12</sup> Resonator RF design

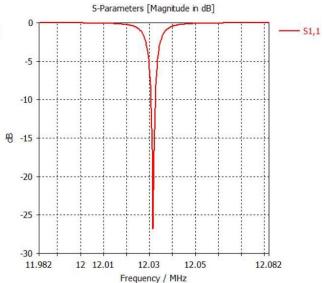


### 6 MHz mode

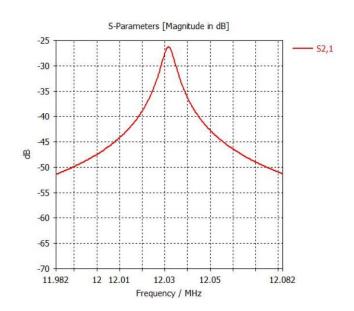




12 MHz mode



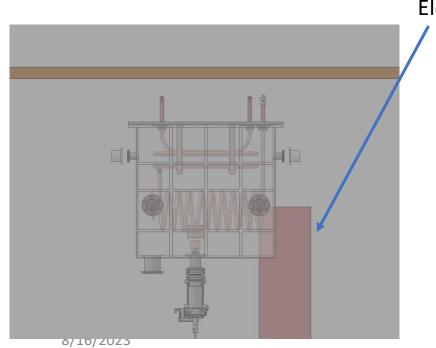
Parameter	6 MHz	12 MHz	
RF power for 150 kV	9500 W	10.8 kW	
Coil dimensions	Coil 1: 7 periods, D=290 mm, H=455 mm, Coil 2: 4.5 periods, D=232 mm, H= 292.5 mm	Coil 2: 4.5 periods, D=232 mm, H= 292.5 mm	
Coil pipe ID/OD	29 mm/35 mm		
Vacuum tank	L×W×H 1280 mm × 750 mm× 1000 mm		
Ground legs pipe ID/OD	44 mm/50 mm		
Кр	4.7 MV/m	5.7 MV/m	
Peak E (150kV)	5.37 MV/m	5.43 MV/m	
Peak E (150kV)/Kp	1.14	0.95	

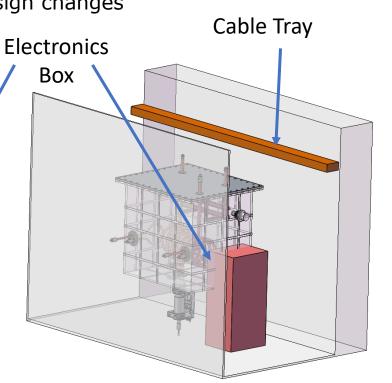


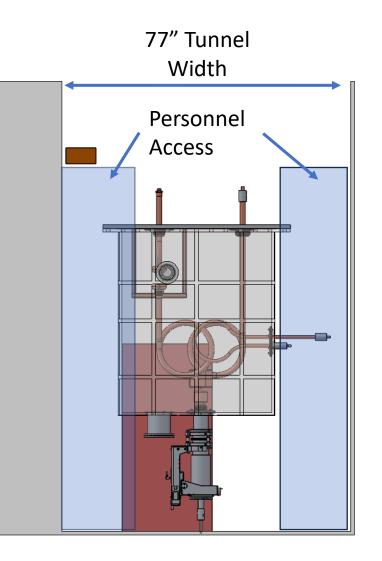
## <sup>13</sup> Engineering design

- Engineering design was ready in 2022, demonstrated good performance, but didn't fit ATLAS tunnel

   Significant redesign required due to previously unknown / unspecified ANL restrictions
- Interferences
  - Electronics box
  - Cable tray
- Beamline tunnel size
  - Personnel access
  - Ceiling limited lifting height
- Underwent several iterations of design changes



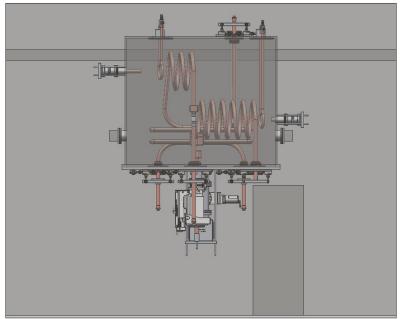


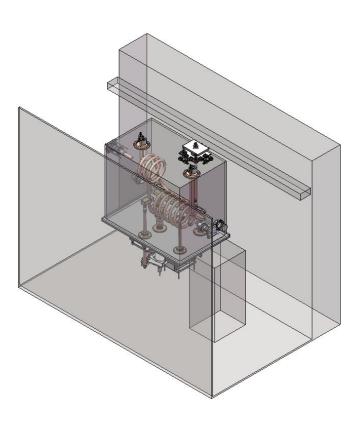


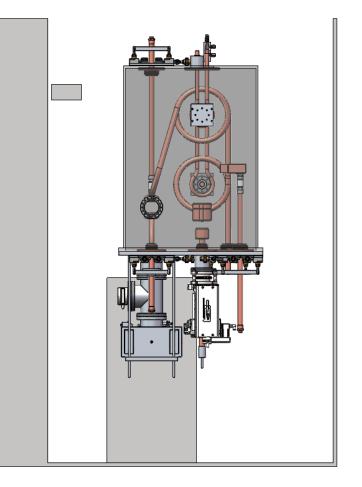


### Redesigned model

- Significantly more compact
   Higher power density...
- Reviewed by ANL and sufficient personnel access reserved
- All interferences resolved
- Conceptual installation plan reviewed



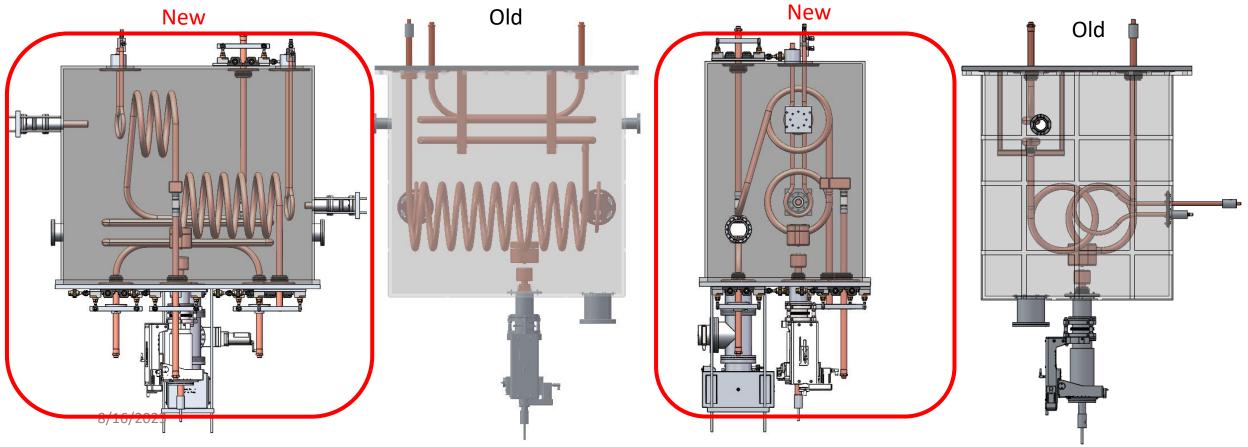






### Latest design summary

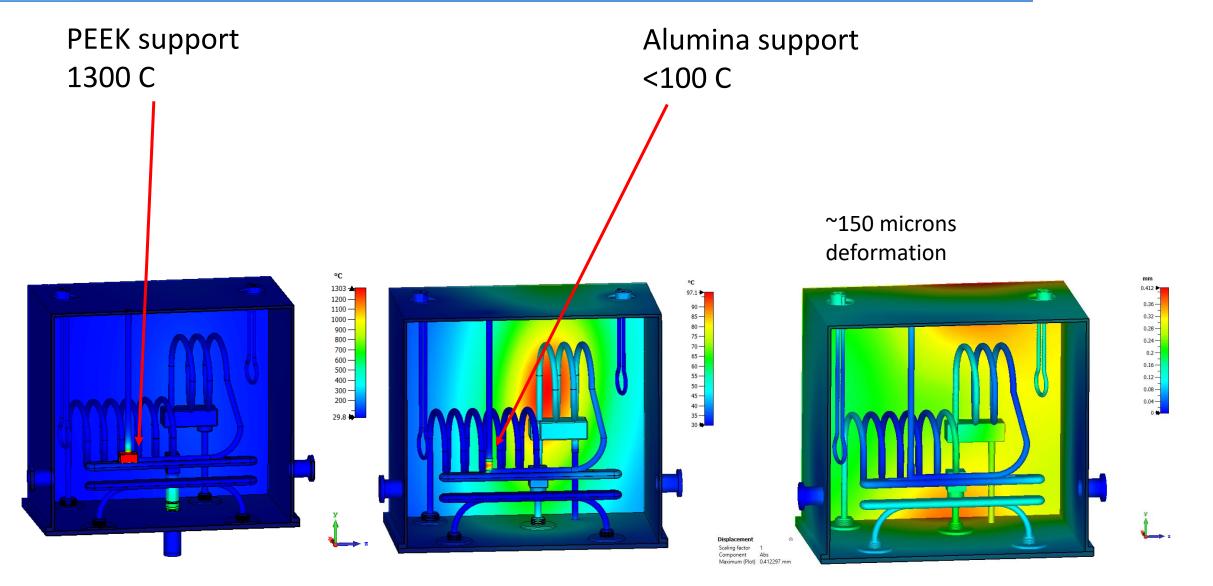
- Main build plate placed on bottom
- Coupling loops placed vertically
- Coils modified and permitted to use water to vacuum braze joints
- Electrode and coil mounts redesigned for alumina vs macor
- Note locations of beampipes





### <sup>16</sup> Last major challenge: electrode support





## <sup>17</sup> Remaining engineering activities

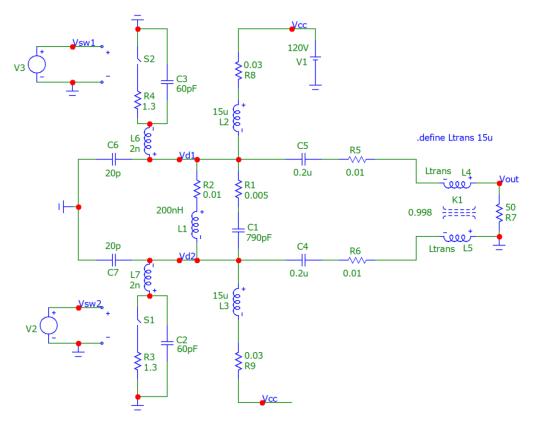


- Detail alumina supports and build testing prototypes
- Incorporate EIA connector detail for power couplers
- Coils (primary and couplers)
  - Add fine features for MFG
    - Forming
    - brazing
  - order material
  - design winding tooling
- Frequency switch
  - Detailed engineering
  - Mechanical test stand development
- Detailed engineering of electrodes to minimize form variance
- Chamber
  - Finalize geometry
  - Perform initial mechanical analysis
  - Generate quoting drawings
  - Begin discussions with vendor and place order
- Design system support stand
- Consider transportation and assembly nuances during all of the above 8/16/2023



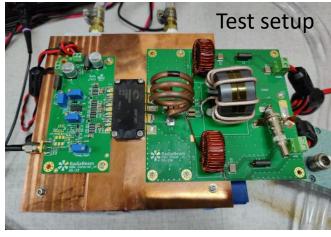
### <sup>18</sup> RF source design

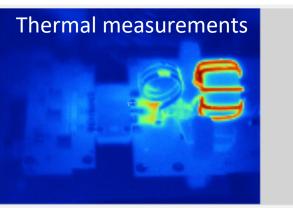
- Push-pull current mode class-D power amplifier
  - Doesn't need an RF transformer, which resulted in a high amplitude of voltage oscillations at the transistors and matching elements.
- 1 kW module is optimal:
  - A further increase in power leads to a drop in efficiency and increases the requirements for the power supply and cooling system
  - We attempted to replace transistors with others with a lower channel resistance (DRF1311) did not lead to improvements. The manufacturer of these transistors made a mistake in the documentation and channel resistance was the same



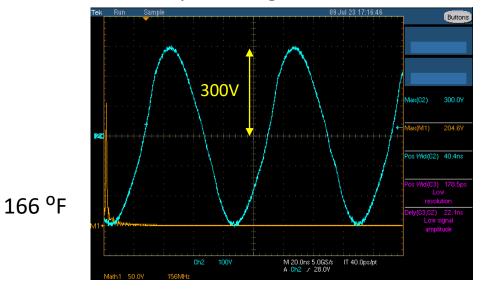
### <sup>19</sup> RF source test results

- We are building 16 kW CW Class-E solid-state amplifiers for 6 and 12 MHz
- 1 kW pallets built and tested at RadiaBeam 87% efficiency achieved;
- Need x16 of both types and 16-to-1 power combiners





Output voltage on 50  $\Omega$  load



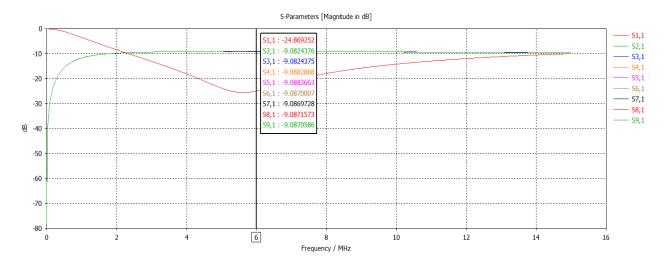
### Measured parameters:

- Frequency: 12.125 MHz
- Input voltage: 130 VDC
- Input current: 8.4 A
- Resonator tank: 250 nH || 600 pF
- Output power: 900 W
- Efficiency: 82.4 %

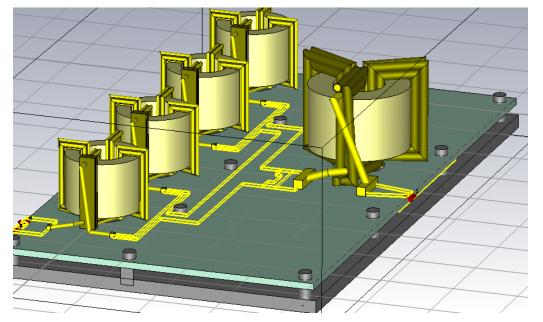


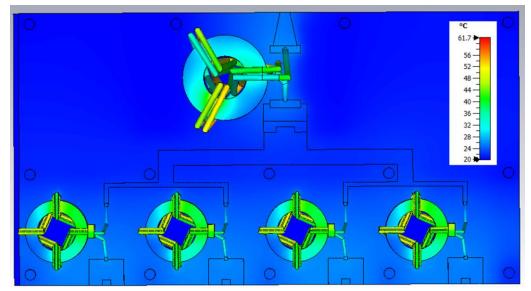
### <sup>20</sup> Power combiner

- 16 1-kW modules will be combined into a single 16 kW module
  - 3-stage binary
  - Transformer-based (RF ferrite)



Scalable design: we can add modules in the future









- The most challenging and ambitious cavity design so far
- Many unexpected obstacles were encountered = delayed progress
- The latest iteration design resolves all problems and been accepted by ANL engineers
- Simulation results are very promising
- Currently, finalizing the engineering features (stand, tuners, fiducials etc.)
- Plan to start fabrication and procurement by Oct. 1
- RF power system is demonstrated and modules are being produced
- NCE will probably be needed, but the success chances are high
- Project Team:
  - Alexander Smirnov, Ronald Agustsson, Aurora Araujo, Evgeny Ivanov and Sergey Kutsaev
- Special acknowledgements:
  - ANL (Brahim Mustapha, Al Barcikowski)
  - DOE NP (Michelle Shinn, Manouchehr Farkhondeh)