

HOM Absorber Design for eRHIC ERL Cavity

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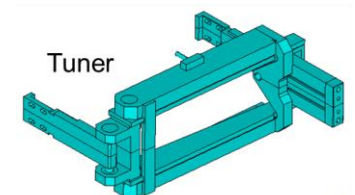
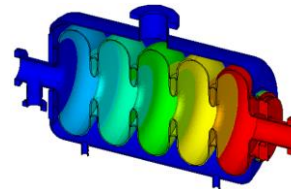
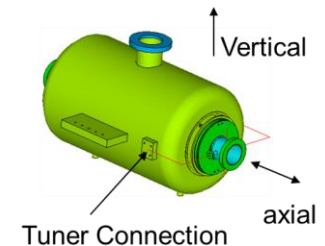
Outline

- TJS Technologies LLC (2016)
 - Engineering Services
 - MSU Michigan State University
 - FRIB ASME evaluation of 644 MHz Cavity and Tuner
 - FHI Fritz Harbor Institute
 - Free Electron Laser Deflector Cavity
 - » RF Thermal Analysis – Design, Coupling
 - JLAB
 - SRF Cavity Cooled by Cryocoolers – Thermal Analysis
 - FPC Coupling to Locate the FPC nearer the cavity
 - » (450kW per FPC)
 - Higher Order Mode Absorber SBIR Phase I & II
 - Waveguide
 - Beamline

Engineering Service MSU

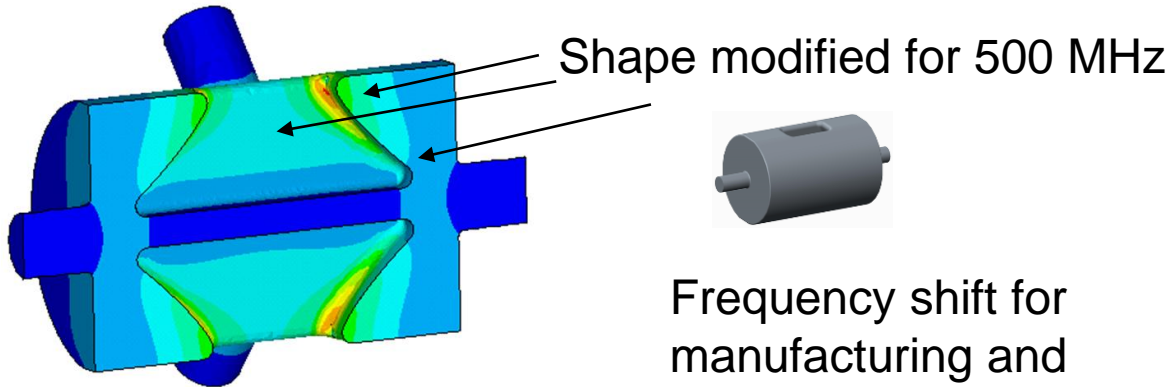
ASME Structural evaluation of FRIB 644 MHz Cavity and Tuner

- **General Requirements of ASME code Section VIII Division 2 – Design by Analysis**
- **Material Properties**
- **Boundary Conditions**
- **Loads to be Considered**
- **Design By Analysis 2015 Section VIII, Division 2 Part 5 of ASME Code**
 - Protection Against Plastic collapse Part 5.2
 - » Limit Load Analysis Part 5.2.3
 - » Elastic-Plastic Analysis Part 5.2.4
 - Protection Against Local failure Part 5.3
 - » Elastic Analysis 5.3.2
 - Protection against collapse From Buckling Part 5.4
 - Bifurcation – Eigenvalue Buckling Part 5.4.1.2
 - Protection Against Failure From Cyclic Loading Part 5.5
 - Experience with comparable equipment operating under similar conditions Part 5.5.2
 - Ratcheting Assessment – Elastic-Plastic Stress Analysis Part 5.5.7
- **Vibration**
- **Frequency Sensitivity to Pressure**
- **Tuner Evaluation**

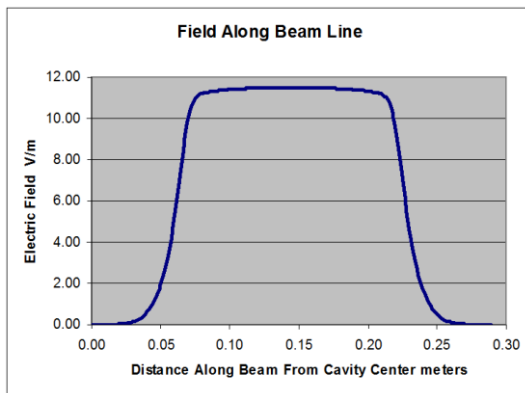


Engineering Service FHI

Develop a Beam Deflector to Provide 2 500 MHz Beams from a single 1 GHz beam
2 Color FEL

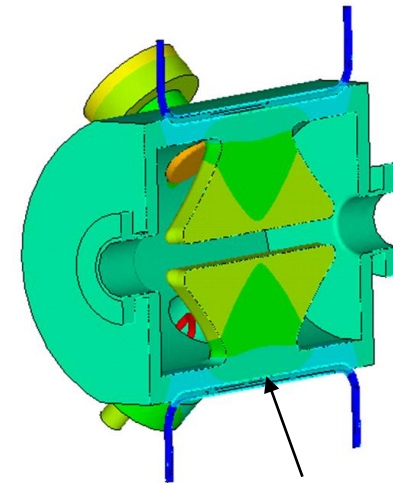


RF Analysis

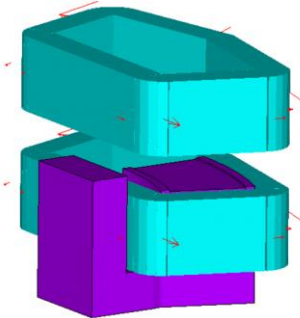


Electric Field Along Beamline

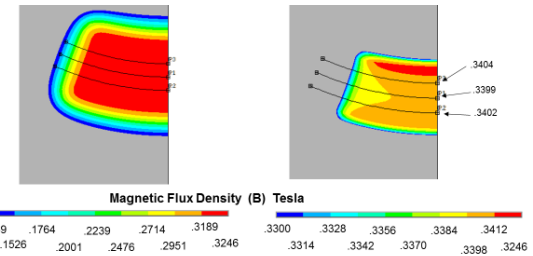
Frequency shift for manufacturing and tuning



Thermal Analysis

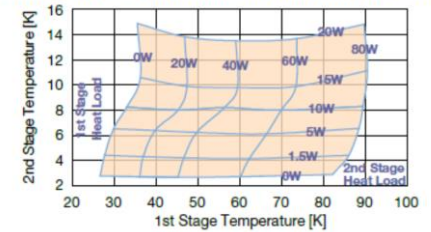
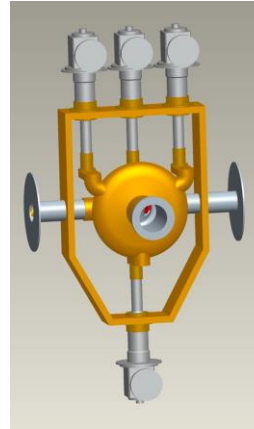
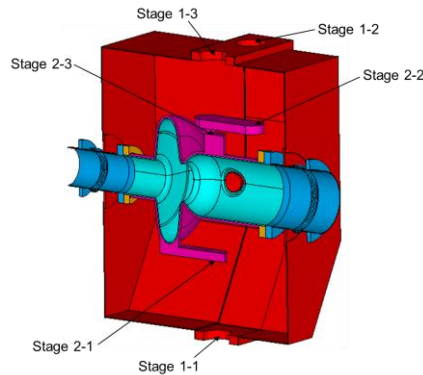
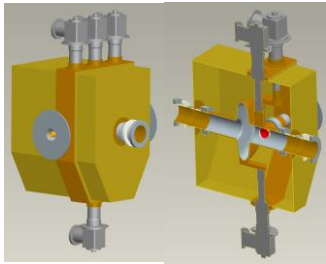


3-D Magnet calcs
Coil geometry
Specification
Field Quality



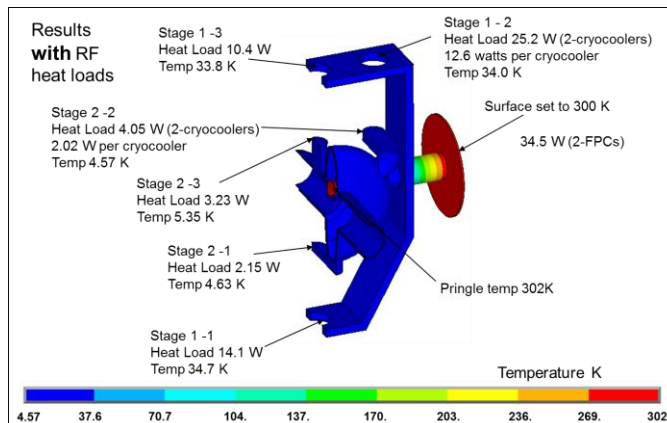
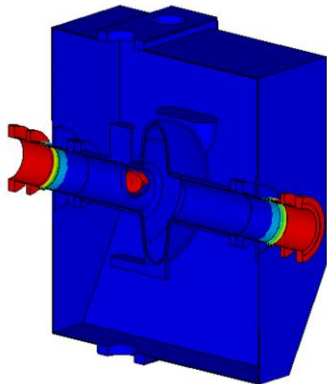
Magnet Analysis

Engineering Service JLAB

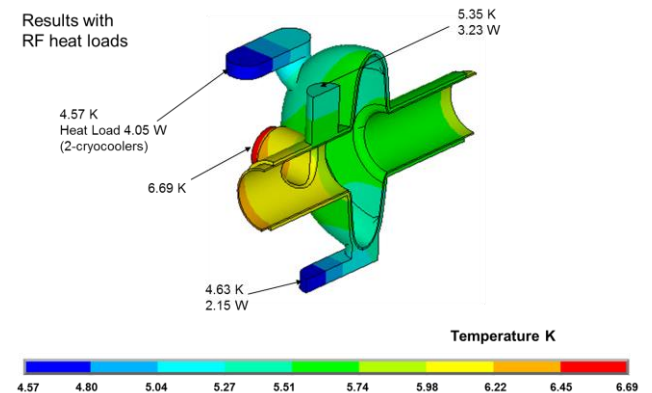


Cryocooler Capacity Map

RF and Thermal Analysis and Coupling for power couplers



Results with RF heat loads



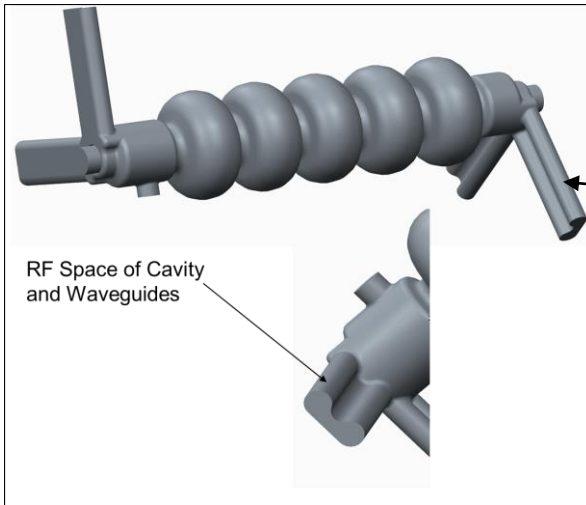
Higher Order Mode Absorber SBIR

- Motivation
 - In 2017 and 2018 BNL was evaluating designs for the electron accelerator in eRHIC, now the EIC, their proposed electron-ion collider
 - It included electron cooling using a multi-cell cavity with high average current and high bunch charge in CW energy recovery mode. This cavity would require a higher order mode absorber with considerable power absorption capability.

Higher Order Mode Absorber SBIR Phase I and Phase II Tasks

- Phase I
 - Define/update HOM specifications with BNL
 - Develop the concept design of the absorber module
 - Perform RF/Thermal and Structural Analysis of the HOM module
 - Develop manufacturing plan and design for the HOM absorber module to a cost level.
- Phase II
 - Manufacture Prototypes
 - Waveguide HOM
 - Beamline HOM

BNL Designed Cavity and B-shaped waveguide



BNL developed a B-Shaped waveguide to suppress multi-pacting and improve impedance decreasing the number of waveguides per cavity
 BNL paper SRF2017 TUPB002

Freq	Power
1.21974E+09	9.66546E+02
1.21036E+09	6.10568E+02
1.23850E+09	5.61609E+02
1.24789E+09	5.33179E+02
1.33233E+09	4.14821E+02
1.22912E+09	4.11329E+02
1.90467E+09	2.60402E+02
1.34171E+09	2.13527E+02
1.30418E+09	1.26510E+02
1.20097E+09	1.26386E+02
1.35110E+09	1.25289E+02
1.36986E+09	1.23914E+02
1.29480E+09	1.12858E+02
1.28542E+09	1.05534E+02
1.27603E+09	1.04885E+02
1.26665E+09	1.02065E+02
1.25727E+09	9.97414E+01
1.31357E+09	9.10959E+01
2.56145E+09	7.79565E+01

BNL supplied a set of HOM Freq with its associated power up to 3.1 GHz where HOM power is 1.2 e-5 W

Table to left is the power sorted by power for the first 19 HOM modes

Table supplied by BNL for freq to 3.13 GHz

For analysis HOM power is not degraded by nearby cavity mode power it is determined from beam frequency and used for design limits making the design conservative

Total Power for Freq to 3.1 GHz is 6.01 kW

Model to Determine Tile Heat Loads with curve and shortened tile length to compact geometry

Driven Model

Input Excitation Port

Frequency Dependent permittivity
and Loss tangent

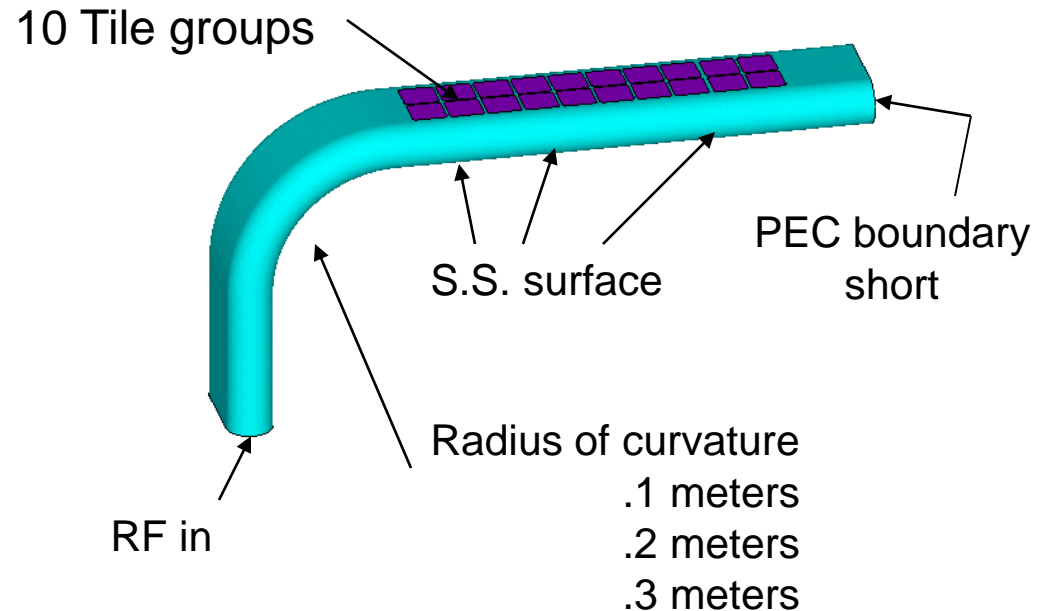
Surface Losses assuming Stainless
Steel

Output

S11, Power for each tile group

For each Frequency

Sum Power for each tile group over
HOM frequencies

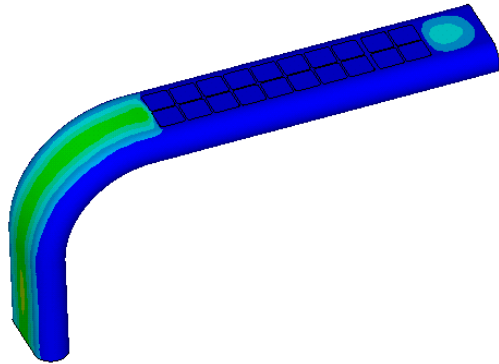


Tile groups with varying thickness
Made from SC-35, graphite loaded

Fields at 1.2197 GHz

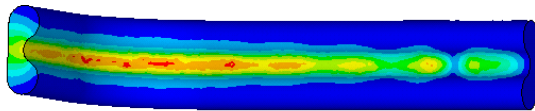
Curved Waveguide Radius .1 meters

Tabulate Results for all evaluated HOMs
4 HOMs per cavity



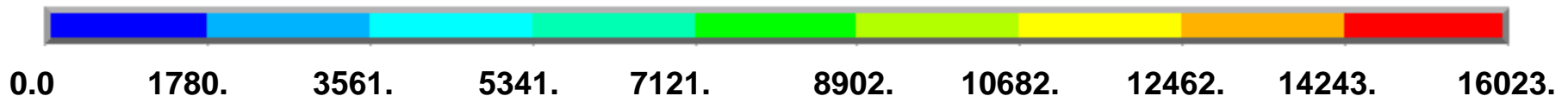
Power 241.6 Watts (966.5/4)
S11 .0363
RefIP .319 W

Freq	Power	S11	RefIP	Surf Loads	Id1	Id2	LD3
1.21974E+09	2.41637E+02	3.63340E-02	3.18999E-01	1.34287E+00	2.05640E+01	2.10396E+01	2.38696E+01
1.21036E+09	1.52642E+02	2.50770E-02	9.59898E-02	8.57093E-01	1.29309E+01	1.27258E+01	1.45691E+01
1.23850E+09	1.40402E+02	6.30190E-02	5.57593E-01	7.64159E-01	1.22239E+01	1.29842E+01	1.51182E+01
1.24789E+09	1.33295E+02	7.37400E-02	7.24802E-01	7.18159E-01	1.18679E+01	1.25528E+01	1.50519E+01
1.33233E+09	1.03705E+02	8.02920E-02	6.68568E-01	5.16512E-01	1.37696E+01	1.05113E+01	1.55004E+01
1.22912E+09	1.02832E+02	5.03010E-02	2.60185E-01	5.65519E-01	8.82375E+00	9.26745E+00	1.05817E+01
1.90467E+09	6.51005E+01	1.17180E-01	8.93905E-01	2.25240E-01	1.63844E+01	1.32115E+01	8.47076E+00
1.34171E+09	5.33818E+01	7.12660E-02	2.71118E-01	2.63818E-01	7.34672E+00	5.55251E+00	8.01851E+00
1.30418E+09	3.16275E+01	9.60880E-02	2.92014E-01	1.61430E-01	3.66959E+00	3.07313E+00	4.51124E+00
1.20097E+09	3.15965E+01	2.84580E-02	2.55887E-02	1.79180E-01	2.66583E+00	2.49959E+00	2.93756E+00
1.35110E+09	3.13223E+01	6.06370E-02	1.15167E-01	1.53636E-01	4.44486E+00	3.36306E+00	4.70684E+00
1.36986E+09	3.09785E+01	3.57750E-02	3.96479E-02	1.49785E-01	4.60074E+00	3.59557E+00	4.60617E+00
1.29480E+09	2.82145E+01	9.73070E-02	2.67153E-01	1.45229E-01	3.11195E+00	2.72818E+00	3.91699E+00
1.28542E+09	2.63835E+01	9.65040E-02	2.45710E-01	1.36982E-01	2.76559E+00	2.54465E+00	3.54499E+00
1.27603E+09	2.62213E+01	9.37260E-02	2.30342E-01	1.37344E-01	2.61716E+00	2.52373E+00	3.39182E+00
1.26665E+09	2.55163E+01	8.90190E-02	2.02201E-01	1.34870E-01	2.43513E+00	2.44740E+00	3.16344E+00
1.25727E+09	2.49354E+01	8.23760E-02	1.69206E-01	1.33040E-01	2.28961E+00	2.37570E+00	2.95315E+00
1.31357E+09	2.27740E+01	9.28180E-02	1.96202E-01	1.15280E-01	2.77424E+00	2.23229E+00	3.31811E+00
2.56145E+09	1.94891E+01	8.87690E-02	1.53573E-01	7.36090E-02	3.76744E+00	3.24892E+00	2.35598E+00

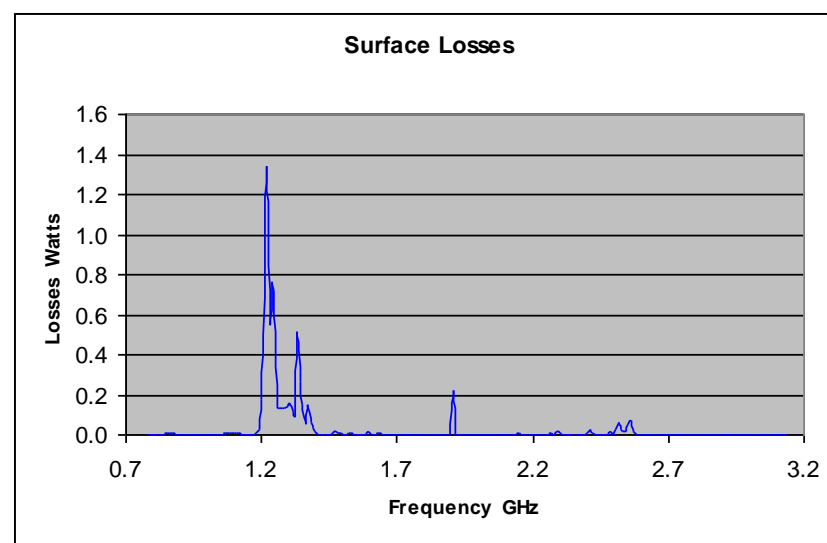
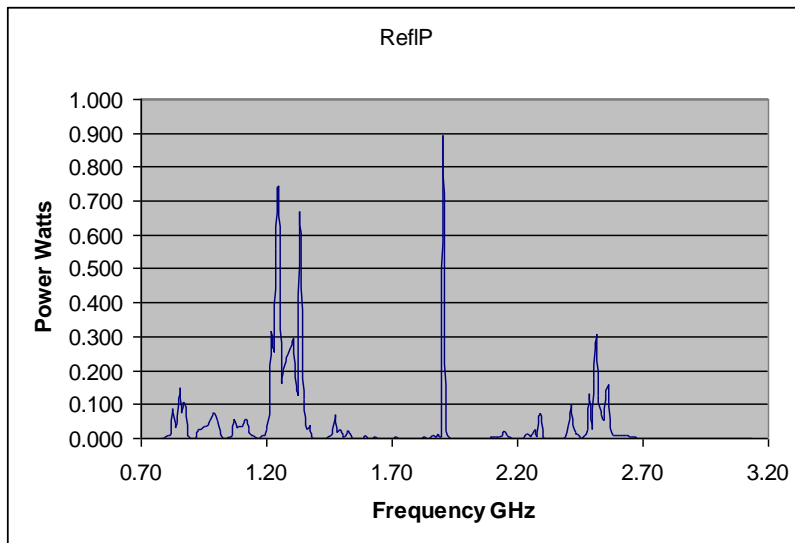
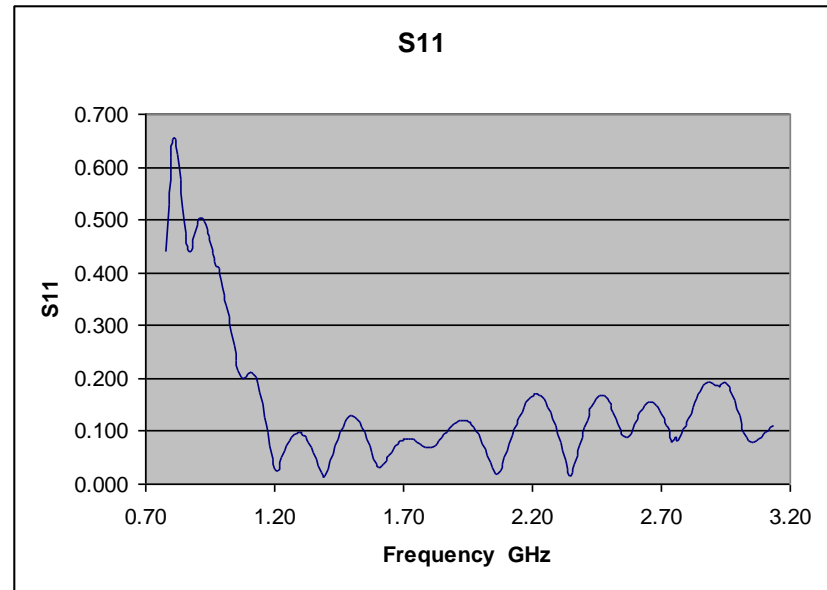
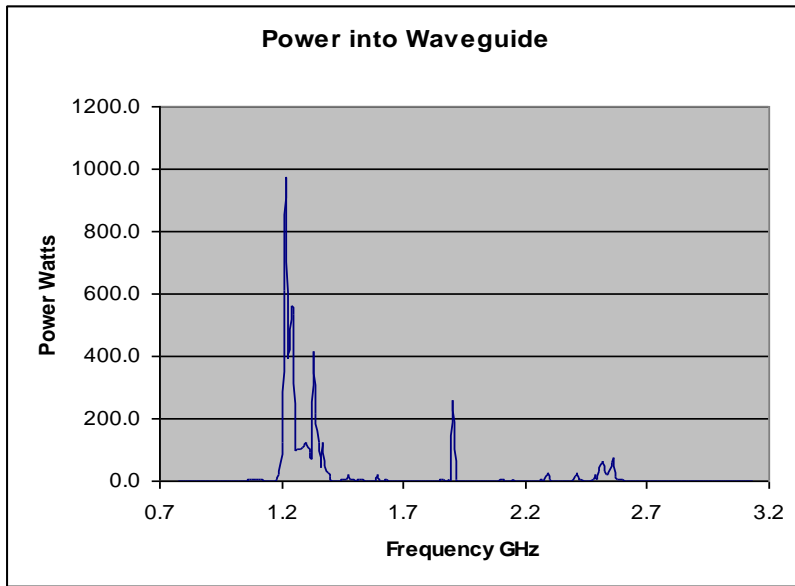


Surface Loss 1.34 W
SS surface elec cond

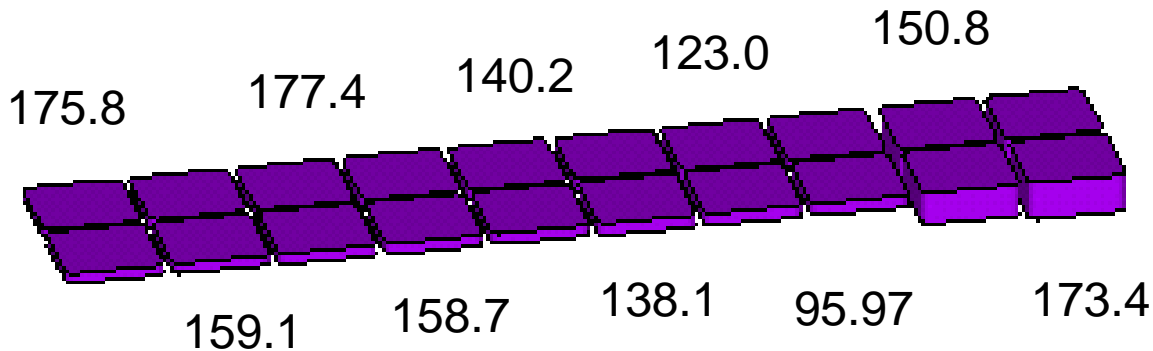
Electric Field V/m



Power In, S11, Reflected Power, Surface Loss



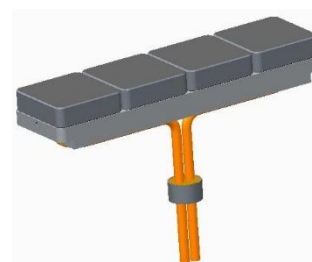
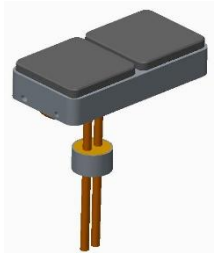
Sum of Power into Waveguide Absorber



- Initial HOM absorber module geometry
 - 1492.4 W of 1501.5 W is absorbed 99.7%
 - 10 tile pairs
 - Thickness range .200" to .75"
 - 2 at .2", 1 at .220", 2 at .225", 3 at .250", 1 at .65", 1 at .75"

Higher Order Mode Absorber SBIR Phase II

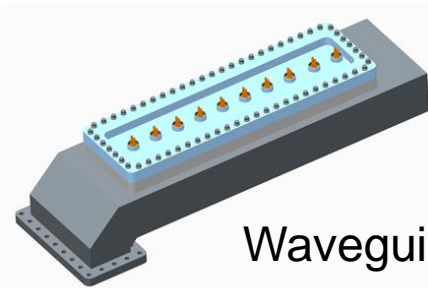
- Manufacture HOM Core
 - Can be used for Waveguide or Beamline Absorber



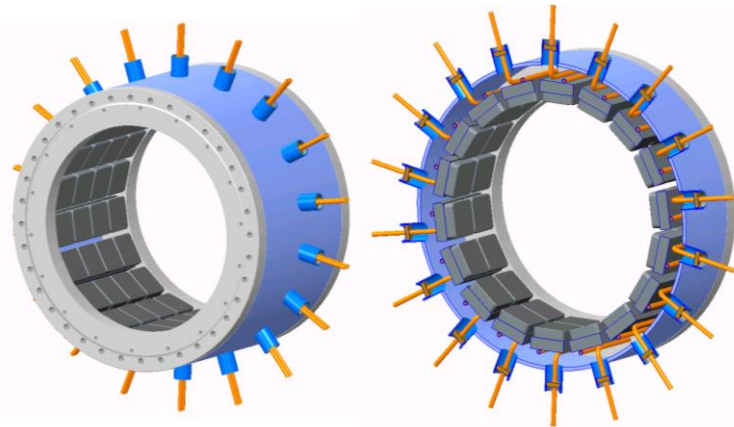
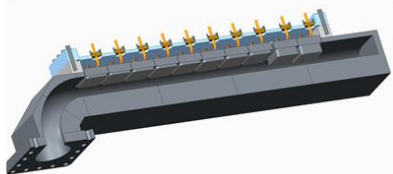
Waveguide core

Beamline core

- Manufacture Housing and Assemble Core and Housing



Waveguide HOM



Beamline HOM

Initial Braze Step in Fabrication of Cores



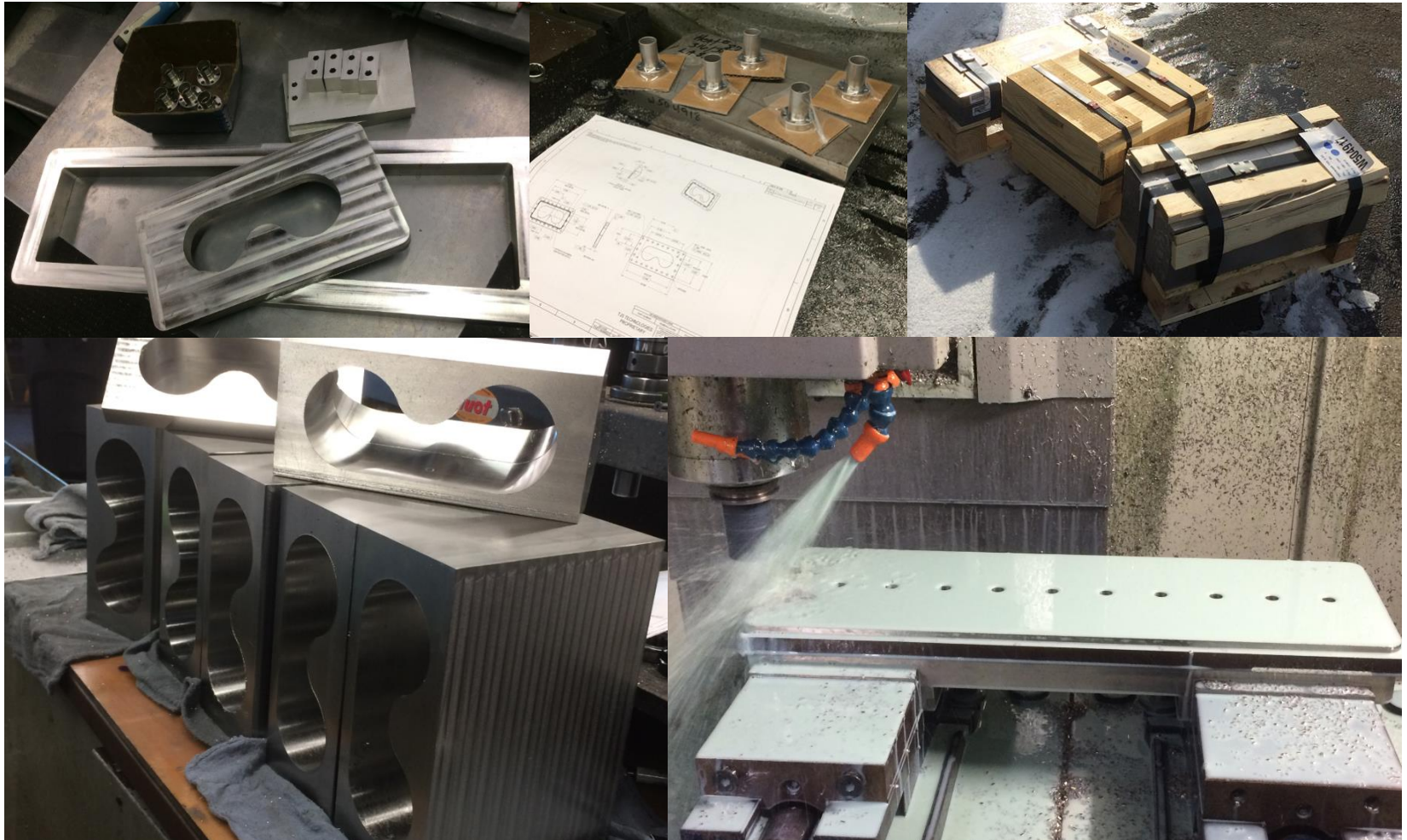
Waveguide Backer Assemblies (without SiC tiles)
Extra assemblies are for Ceramic joining tests

Join Ceramic Tiles to Backers



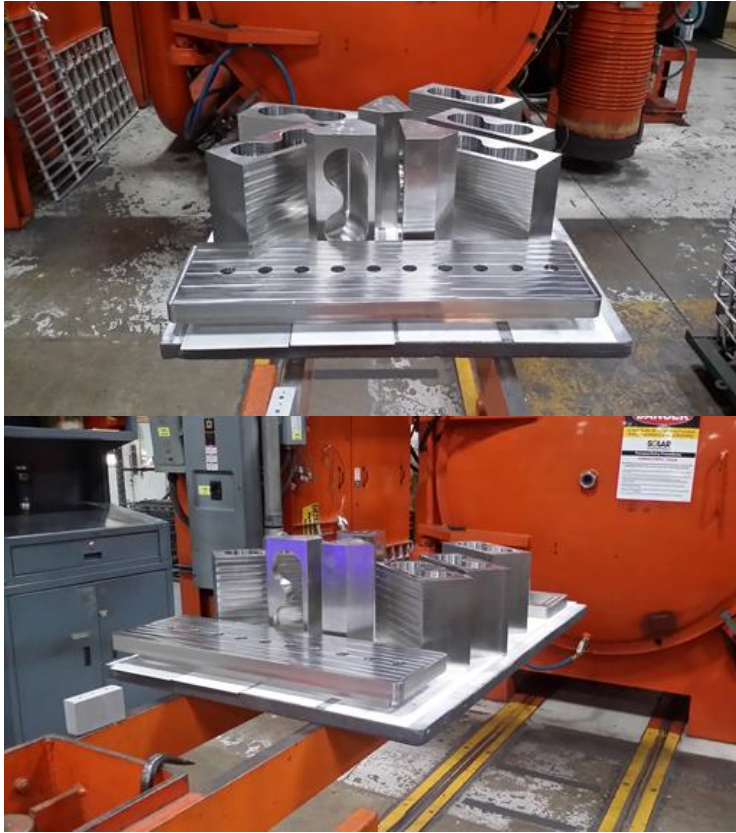
Backer-Tile Assemblies shown after joining

Machining of Waveguide Assembly

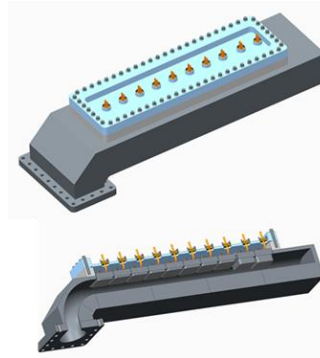


Machining of Waveguide Housing Parts

Higher Order Mode Absorber SBIR Phase II



Waveguide parts after heat treat (annealing). Prior to final machining.



Parts stacked with braze alloy - thermocouples applied, ready for intermediate braze step

SBIR Summary

- On Track to complete waveguide and Beamline HOM Absorber by end of Yr2
- Using HOM core can develop many geometries to accomplish HOM absorption
- Size of beampipe absorber can be accommodated by adding more cores circumferentially